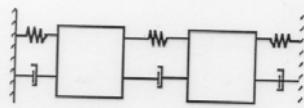


Analytical and Experimental Modal Analysis

Signal Processing: Modal Analysis

Modal description of vibrating system

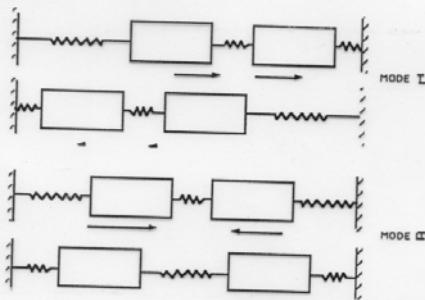


Two deflection shapes exist for each eigenfrequency.

They are described by the modal matrix

Deflection shapes are eigenvectors of modal matrix

$$\begin{bmatrix} \Phi_{11} & \Phi_{12} \\ \Phi_{21} & \Phi_{22} \end{bmatrix} = [(\Phi)_1 (\Phi)_2]$$

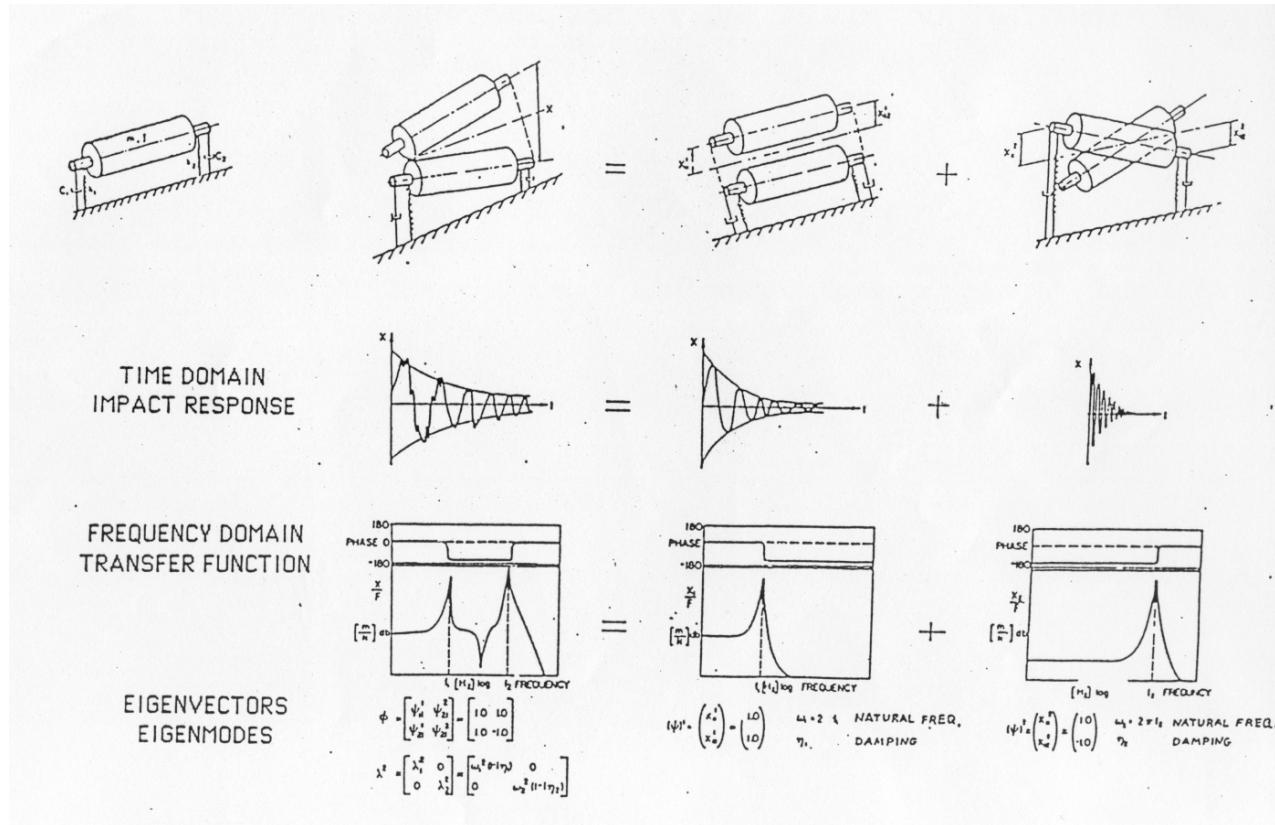


$$(\Phi)_r = \begin{bmatrix} \Phi_{r1} \\ \Phi_{r2} \end{bmatrix}$$

The eigenvalue matrix describes natural frequencies

$$\begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_2 \end{bmatrix}$$

$$\lambda_r = \omega_r^2$$



Signal Processing: Modal Analysis

$$m_1 \ddot{x}_1 + c_1 \dot{x}_1 + c_2 (\dot{x}_1 - \dot{x}_2) + k_1 x_1 + k_2 (x_1 - x_2) = f_1$$

$$m_2 \ddot{x}_2 + (c_2 + c_3) \dot{x}_1 + (k_2 + k_3) x_2 - c_2 \dot{x}_1 - k_2 x_1 = f_2$$

$$m_1 \ddot{x}_1 + (c_1 + c_2) \dot{x}_1 + (k_1 + k_2) x_1 - c_2 \dot{x}_2 - k_2 x_2 = f_1$$

$$m_2 \ddot{x}_2 + c_2 (\dot{x}_2 - \dot{x}_1) + k_3 x_2 + k_2 (x_2 - x_1) = f_2$$

$$[m] = \begin{bmatrix} m_1 & 0 \\ 0 & m_2 \end{bmatrix} \quad [c] = \begin{bmatrix} c_1 + c_2 & -c_2 \\ -c_2 & c_2 + c_3 \end{bmatrix} \quad [k] = \begin{bmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 + k_3 \end{bmatrix}$$

$$(x) = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} \quad (\dot{x}) = \begin{pmatrix} \dot{x}_1 \\ \dot{x}_2 \end{pmatrix} \quad (\ddot{x}) = \begin{pmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{pmatrix} \quad (f) = \begin{pmatrix} f_1 \\ f_2 \end{pmatrix}$$

General: $[m](\ddot{x}) + [c](\dot{x}) + [k](x) = (f)$

$$m(N \times N) \quad c(N \times N) \quad x(N \times 1) \quad f(N \times 1)$$

Undamped system:

$$[c] = 0$$

$$(\ddot{x}) = -\omega^2(\psi) \exp(j\omega t)$$

$$-\omega^2 [m](\psi) + [k](\psi) = 0$$

$$-\lambda[m](\psi) + [k](\psi) = 0$$

$$\{[m]^{-1}[k] - \lambda[I]\}(\psi) = 0$$

λ_i eigenvalue

$(\psi)_i$ eigenvector

$$m_1 = 5 \text{ kg} \quad m_2 = 10 \text{ kg} \quad k_1 = k_2 = 2N/m \quad k_3 = 4N/m$$

$$\left| \begin{bmatrix} 5 & 0 \\ 0 & 10 \end{bmatrix}^{-1} \begin{bmatrix} 4 & -2 \\ -2 & 6 \end{bmatrix} - \lambda \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \right| = 0 \quad (4/5 - \lambda)(3/5 - \lambda) - (-1/5)(-2/5) = 0$$

$$\lambda_1 = 2/5 \quad \omega_1 = (2/5)^{1/2} \quad [\text{rad/sec}]$$

$$\lambda_2 = 1 \quad \omega_2 = 1 \quad [\text{rad/sec}]$$

$$\lambda_1 = \omega_1^2 = 2/5 \quad \begin{bmatrix} 4/5 - 2/5 & -2/5 \\ -1/5 & 3/5 - 2.5 \end{bmatrix} \begin{pmatrix} \Psi_{11} \\ \Psi_{21} \end{pmatrix} = \begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

$$2/5 \Psi_{11} - 2/5 \Psi_{21} = 0$$

$$\Psi_{11} = \Psi_{21}$$

$$(\Psi)_1 = \begin{pmatrix} \Psi_{11} \\ \Psi_{21} \end{pmatrix} = \begin{pmatrix} \Psi_{11} \\ \Psi_{11} \end{pmatrix}$$

$$\lambda_2 = \omega_2^2 = 1 \quad (\Psi)_2 = \begin{pmatrix} \Psi_{12} \\ -\frac{1}{2}\Psi_{12} \end{pmatrix}$$

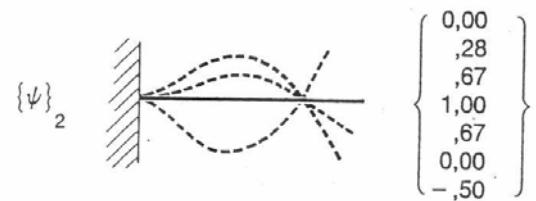
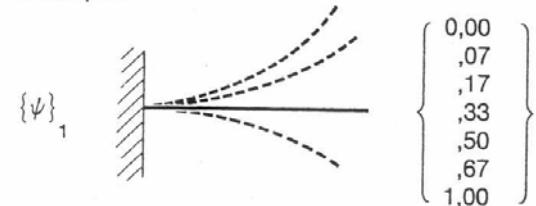
Multi Degree of Freedom Models

• Mode Shape

$$[B(p_r)] \{X\}_r = \{0\} \quad (1)$$

$\{X\}_r = \{\psi\}_r$ mode shape for mode # r

Example:



$\{\psi\}_r$ is solution for homogenous equation (1), i.e. only the relative deflections are found



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$$\lambda_i \neq \lambda_j \quad (\psi)_i^T [m](\psi)_j = 0$$

$$(\psi)_i^T [k](\psi)_j = 0$$

$$\lambda_i = \lambda_j \quad (\psi)_i^r [m](\psi)_i = M_i$$

$$(\psi)_i^T [k](\psi)_i = K_i$$

$$[\psi]^T [m] [\psi] = \begin{bmatrix} & & \\ & M_i & \\ & & \end{bmatrix}$$

Weighted Orthogonality relations

$$[\psi]^T [k] [\psi] = \begin{bmatrix} & & \\ & K_i & \\ & & \end{bmatrix}$$

$$K/M_i = \omega_i^2$$

Generalized mass and stiffness

$$\omega_1 = (2/5)^{1/2} \quad \text{set } \psi_{11} = 1 \quad (\psi)_1 = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$$

$$\begin{pmatrix} 1 \\ 1 \end{pmatrix}^T \begin{bmatrix} 5 & 0 \\ 0 & 10 \end{bmatrix} \begin{pmatrix} 1 \\ 1 \end{pmatrix} = M_1 = 15$$

$$K_1 = \omega_1^2 M_1 = 6 \quad \omega_2 = 1 \quad \text{Set } \psi_{12} = 1 \quad (\psi)_2 = \begin{pmatrix} 1 \\ -\frac{1}{2} \end{pmatrix}$$

$$\begin{pmatrix} 1 \\ -\frac{1}{2} \end{pmatrix}^T \begin{bmatrix} 5 & 0 \\ 0 & 10 \end{bmatrix} \begin{pmatrix} 1 \\ -\frac{1}{2} \end{pmatrix} = M_2 = 15/2$$

$$K_2 = \omega_2^2 M_2 = 15/2$$

$$[M] = \begin{bmatrix} 15 & 0 \\ 0 & 15/2 \end{bmatrix} \quad [K] = \begin{bmatrix} 6 & 0 \\ 0 & 15/2 \end{bmatrix}$$

$$M_i = I$$

$$K_i = \omega_i^2 M_i = \omega_i^2$$

$$\omega_1 = (2/5)^{1/2} \quad \begin{pmatrix} \phi_{11} \\ \phi_{21} \end{pmatrix}^T \begin{bmatrix} 5 & 0 \\ 0 & 10 \end{bmatrix} \begin{pmatrix} \phi_{11} \\ \phi_{21} \end{pmatrix} = M_1 = 1$$

$$\phi_{11} = \phi_{21}$$

$$(\phi)_1 = \begin{pmatrix} \sqrt{1/15} \\ \sqrt{1/15} \end{pmatrix}$$

$$\omega_2 = 1 \quad \begin{pmatrix} \phi_{12} \\ \phi_{22} \end{pmatrix}^T \begin{bmatrix} 5 & 0 \\ 0 & 10 \end{bmatrix} \begin{pmatrix} \phi_{12} \\ \phi_{22} \end{pmatrix} = M_2 = 1$$

$$(\phi)_2 = \begin{pmatrix} \sqrt{2/15} \\ -0.5\sqrt{2/15} \end{pmatrix}$$

$$(\phi)_i = \frac{1}{\sqrt{M_i}} (\psi)_i$$

**Mass normalized
eigenvectors**

$$[\psi] = [(\psi)_1 \dots (\psi_2) \dots (\psi_n)]$$

$$(x) = [\psi]q \quad q = [\psi]^{-1}(x)$$

Generalized coordinates

$$[m](\ddot{x}) + [k](x) = (f)$$

$$[\psi]^T [m][\psi](\ddot{q}) + [\psi]^T [k][\psi](q) = [\psi]^T(f)$$

$$[M](\ddot{q}) + [K](q) = [\psi]^T(f)$$

$$M_i \ddot{q}_i + K_i q_i = (\psi)_i(f) = f_i$$

$$\ddot{q}_i + \omega_i^2 q_i = f_i / M_i = \frac{(\psi)_i^T(f)}{(\psi)_i^T [m](\psi)_i}$$

$$\ddot{q}_i + \omega_i^2 q_i = f_i = (\phi)_i^T(f)$$

$$[\psi] = \begin{bmatrix} 1 & 1 \\ 1 & -\frac{1}{2} \end{bmatrix}$$

$$(x) = [\psi]q = \begin{pmatrix} x_1 \\ x_2 \end{pmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & -\frac{1}{2} \end{bmatrix} \begin{pmatrix} q_1 \\ q_2 \end{pmatrix}$$

$$[\psi]^T [m] [\psi] = \begin{bmatrix} 15 & 0 \\ 0 & -\frac{1}{2} \end{bmatrix}$$

$$[\psi]^T [k] [\psi] = \begin{bmatrix} 6 & 0 \\ 0 & \frac{15}{0} \end{bmatrix}$$

$$\begin{bmatrix} 15 & 0 \\ 0 & 15/2 \end{bmatrix} + \begin{pmatrix} \ddot{q}_1 \\ \ddot{q}_2 \end{pmatrix} + \begin{bmatrix} 6 & 0 \\ 0 & \frac{15}{2} \end{bmatrix} \begin{pmatrix} q_1 \\ q_2 \end{pmatrix} = \begin{bmatrix} 1 & 1 \\ 1 & -\frac{1}{2} \end{bmatrix} \begin{pmatrix} f_1 \\ f_2 \end{pmatrix}$$

$$15\ddot{q}_1 + 6q_1 = f_1 + f_2$$

$$\frac{15}{2}\ddot{q}_1 + \frac{15}{2}q_2 = f_1 - \frac{f_2}{2}$$

Uncoupling of equations

$$m\ddot{x} + kx = f \exp(j\omega t)$$

$$(k - \omega^2 m)x = f$$

Transfer Function approach

$$\{[k] - \omega^2 [m]\}(x) = (f)$$

$$[H]^{-1}(x) = (f) \quad (x) = [H](f)$$

$$[H]^{-1} = [k] - \omega^2 [m]$$

$$[\phi]^T [H]^{-1} [\phi] = [\phi]^T [k] [\phi] = \omega^2 [\phi]^T [m] [\phi] = \begin{bmatrix} \backslash & & \\ & \omega_r^2 - \omega^2 & \\ & & \backslash \end{bmatrix}$$

$$[H] = [\phi] \begin{bmatrix} \backslash & & \\ & \omega_r^2 - \omega^2 & \\ & & \backslash \end{bmatrix}^{-1} [\phi]^T$$

$$f = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ f_k \\ 0 \end{pmatrix} \quad (x) = \begin{bmatrix} \phi_{11} & \phi_{12} & \cdots & \phi_{1N} \\ \phi_{21} \\ \vdots \\ \phi_{N1} & & & \phi_{NN} \end{bmatrix} \begin{bmatrix} \backslash & & & \\ & (\omega_r^2 - \omega^2) & & \\ & & \backslash & \end{bmatrix}^{-1} \begin{bmatrix} \phi_{11} & \phi_{21} & \cdots & \phi_{N1} \\ \phi_{12} \\ \vdots \\ \phi_{1N} & & & \phi_{NN} \end{bmatrix} = \begin{pmatrix} 0 \\ 0 \\ \vdots \\ f_2 \\ 0 \end{pmatrix}$$

$$\begin{pmatrix} x_1 \\ x_2 \\ \vdots \\ x_N \end{pmatrix} = \begin{bmatrix} \phi_{11} & \phi_{12} & \cdots & \phi_{1N} \\ \vdots \\ \phi_{N1} & & & \phi_{NN} \end{bmatrix} \begin{bmatrix} \backslash & & & \\ & (\omega_r^2 - \omega^2) & & \\ & & \backslash & \end{bmatrix}^{-1} \begin{pmatrix} \phi_{k1} \\ \phi_{k2} \\ \vdots \\ \phi_{kN} \end{pmatrix} f_k$$

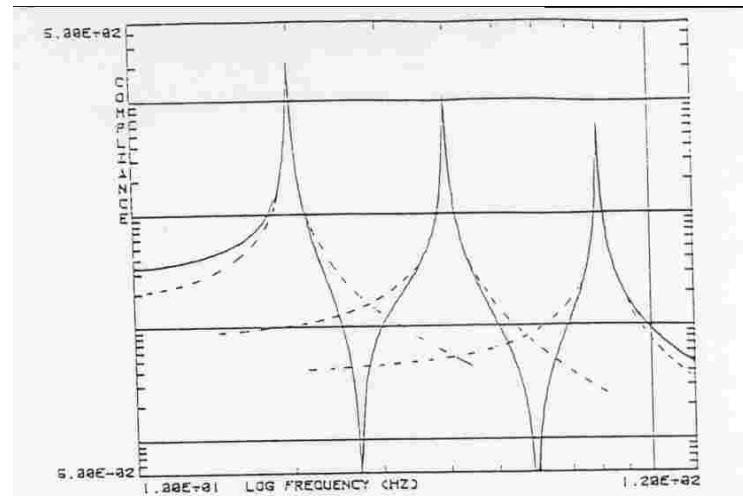
$$x_i = (\phi_{i1} \phi_{i2} \dots \phi_{iN}) \begin{bmatrix} \backslash & & & \\ & (\omega_r^2 - \omega^2) & & \\ & & \backslash & \end{bmatrix}^{-1} \begin{pmatrix} \phi_{k1} \\ \vdots \\ \phi_{kN} \end{pmatrix} f_k$$

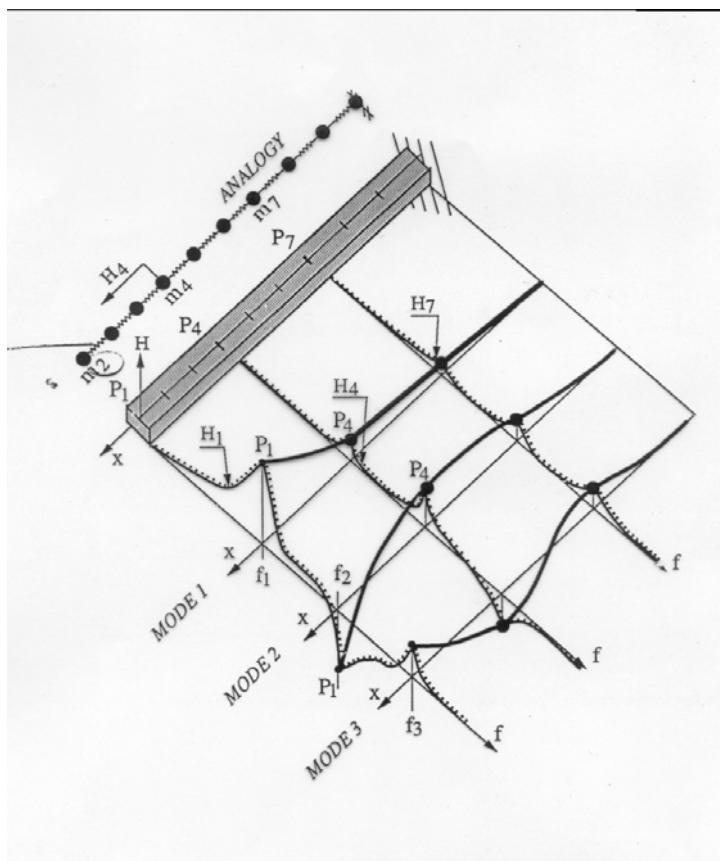
Summary:

$$H_{ik} = \sum_{r=1}^N \frac{\phi_{ir}\phi_{kr}}{\omega_r^2 - \omega^2}$$

$$H_{ik} = \sum_{r=1}^N \frac{\phi_{ir}\phi_{kr}}{\omega_r^2 - \omega^2 + j2\varepsilon_r\omega_r\omega} = \sum_r \frac{\nu A_{ik}}{\omega_r^2 - \omega^2 + j^2\varepsilon_r\omega_r\omega}$$

$$\nu A_{ik} = \phi_{ir}\phi_{kr}$$

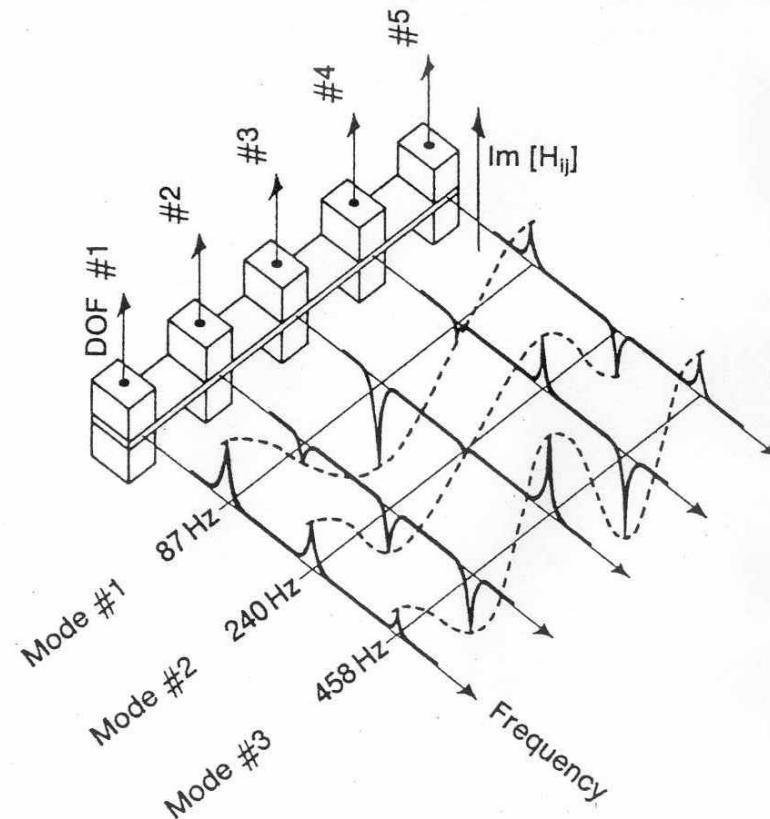




Signal Processing: Modal Analysis

Frequency Response Function and Modal Parameters

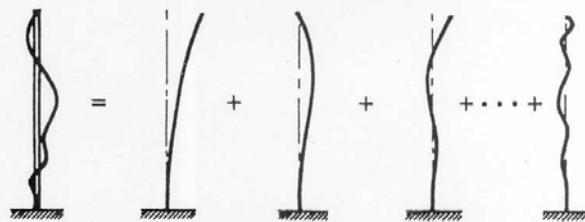
• Mode Shapes from Quadrature Picking



Modal Analysis Introduction

Modal Behaviour

- The dynamic response of a structure can be decomposed into a discrete set of independent particular motions
- These motions are called Modes of Vibration
- A Mode is described by the Modal Parameters:
 - * Natural Frequency & Damping
 - * Mode Shape



$$x(y,t) = q_1(t) \{ \phi \}_1 + q_2(t) \{ \phi \}_2 + q_3(t) \{ \phi \}_3 + \dots + q_n(t) \{ \phi \}_n$$

- Modal Analysis is the process of determining the modal parameters and ultimately to
- Create a mathematical Model



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Modal Analysis Introduction

- Mathematical Models

- Wave Equation

A diagram showing a beam of length x with a vertical axis y . A force $p(t)$ is applied at the top of the beam, represented by several upward arrows. The beam is fixed at the bottom.

$$\frac{\partial^2}{\partial x^2} \left[I E(x) \frac{\partial^2 y}{\partial x^2} \right] + m(x) \frac{\partial^2 y}{\partial t^2} =$$

- Lumped Parameters

A diagram of a mechanical system consisting of a rectangular mass connected to four springs, each attached to a fixed base. A downward arrow indicates a force or displacement.

$$[m] \{ \ddot{x} \} + [c] \{ \dot{x} \} + [k] \{ x \} =$$

- Finite Elements

A diagram showing a beam discretized into two elements. The left part shows a single element, and the right part shows a more complex truss-like element with multiple nodes and springs.

$$[m] \{ \ddot{x} \} + [k] \{ x \} = \{ f \}$$

$$[k]_{2 \times 2} \quad [k]_{18 \times 1}$$

- Experimental Modal Model

A diagram of a car with a sensor icon and a block labeled $[H]$. Below the car is a block labeled $\{F\}$.

$$\{X\} \quad \{X\} = [H] \{F\}$$

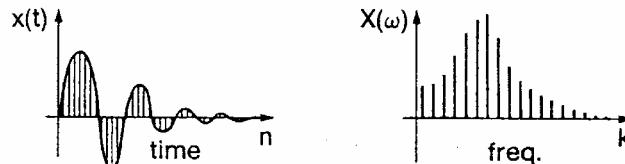
$$[H] = \sum_r^{2m} \frac{\{\psi\}_r \{\psi\}_r^T}{j\omega_r + \sigma_r - j\omega_{dr}}$$

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The Modal Transformation

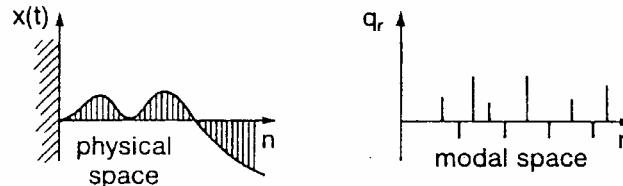
• Fourier – vs. Modal Transformation

Fourier



or $x(t) = [e^{j\omega t}] \{X(\omega)\} = \sum_{n=1}^{N/2} \sin(\omega_n t) \times X_n$

Modal



or $\{x\} = [\Phi] \{q\} = \sum_{r=1}^m \{\phi\}_r \cdot q_r$

Imagine:

$$[e^{j\omega t}] = [| \langle \langle \cdots \rangle \rangle] \quad \text{and} \quad \Phi = [\{ \} \{ \} \cdots \{ \}]$$



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